Electronics Park Syracuse, New York February 18, 1955

Subject: Lacquer Studies

The following report is the result of preliminary laboratory work done in attempting to set up a method of evaluating the nitro-cellulose lacquer in present use.

Certain chemical and physical tests were performed on each of the three components of the lacquer, to arrive at some limitations on their acceptability.

This report is meant to serve only as a guide. Additional tests and refinements of existing procedures will be reported as they develop.

Victor G. Betar Paul L. Dec

Victor Betar

Paul L. Dee

Materials and Processes
CATHODE-RAY TUBE SUB-DEPARTMENT

idh

Distribution:

R. H. Porg

W. H. Eertrand

J. G. Cretekos

G. W. Cavanaugh, Building #3, Room 3

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P. F. Marapodi

M. J. Ozeroff

A. N. Reagan

R. Rusek, Buffalo Tube Plant

I. J. Steinhardt, Buffalo Tube Plant

EVALUATION OF SOLVENTS

Distillation
A 15 inch distilling column packed with unglazed porcelain is used.
A controlled heat source (electric mantle) is necessary. A water cooled condenser will be satisfactory to condense the vapors.

Place 100 so of the solvent into a round bottom flask. Drop in a few boiling chips. Assemble the remaining apparatus and apply heat. The column may have to be insulated (aluminum foil) to enable the vapors to reach the take off arm. As vapors start to condense, adjust the heat to allow a steady take off rate of about 2 drops per second. Record the temperature of the first drop and at intervals of 10sc until no further distillate comes over. Collect each 10sc fraction in a separate bottle. Additional heat may be required as the distillation progresses.

By comparing the specific gravity* of the solvent and the boiling range and refractive indecies of each fraction with the data compiled on known mixtures, it is possible to approximate the composition of the solvent. To be usable, the ester content should be 90% or greater.

For example, in determining the composition of an unknown solvent after the following information is obtained:

Initial Specific gravity - 0,864 at 23°C

ls	t drop	128°C	N25
		÷	D
	10	132	1.3945
	20	134	1.3952
	30	135	1.3959
	40	136	1.3965
	50	137	1.3968
	60	137	1,3972
	70	138	1.3976
	80	139	1.3980
	90	140	1.3984
	Pot.	est .	1.3988

The following analysis can be used:

Comparing the results with those on chart number 1, we find that the specific gravity compares favorably with mixtures 4, 5, and 6. This tentatively eliminates mixtures 1, 2, and 3 even though their fractions have refractive indecies fairly close to these in the unknown. The boiling ranges of 1, 2, and 3 also would be such as to disqualify their consideration.

Closer examination of the boiling range data on mixtures 4, 5, and 6 tends to indicate that the unknown compares closest to mixture number 5.

Therefore, first by comparing the specific gravity and then by further comparing the boiling range and the refractive indecies, a fairly close approximation of the unknown can be made.

It is quite evident from the data compiled on the various mixtures that:

- 1. The specific gravity tends to decrease as the alcohol content increases.
- 2. The refractive indesies of the first fractions are lower when the mixture is richer in iso butyl acetate or butyl alcohol.
- 3. The boiling ranges of the 90% ester content mixtures are in the 130-140 °C. neighborhood where as those of less ester content are in the 120-135°C range.

As a final check on the ester content of the solvent, reference should be made to the section on neutralization.

Description of Apparatus

15" distillation column Will Cat. #11966 20" water cooled condenser Will Cat. #9636 100 ec round bottom flask 25-200°C thermometer 100 ec Heating Mantle Will Cat. #15981 Unglazed porcelain Collecting bottles Abble Refractometer Will Cat. #23001 Constant Temp. Bath. Will Cat. #28521

* The specific gravity was taken with an araometer at 23°C. Scale 0,8500-1,000

Ester Hydrolysis (Nautralization)

On an analytical balance, weigh out approximately 1 gram of solvent in a weighing bottle. Pour it into a 1000cc round bottom flask. Pipette 25cc of 1N KOH (alcoholic) into the weighing bottle and pour into the flask also. Rinse the bottle with 10cc of ethyl alcohol and add to the flask. Place the flask on a heating mantle and insert a vertical water cooled condenser into the mouth. Apply heat slowly and reflux for one hour taking care not to lose any of the vapors out the top of the condenser. Refluxing of about 1 drop per second is sufficient.

After refluxing for 1 hour cool to room temperature. Add a few drops of phenolphthlein to the flask and titrate with 1N HCL.

Reaction:

RCOR KOLL RCOH + ROH

JKOH

RCOK + HO

Weight of ester = (mlKOH - mlHCl) Milli Equiv. Wt. Ester

% Ester = (wt. of ester) 100 (wt. of solvent) Milli equiv. wt. of amyl acetate = 130

NOTE: Only valid when Normality of KOH = Normality of HCL.

Determination of Free Acid - (CH COOH)

Pour 200ce of solvent in a separatory funnel, add 200ce of deionized water. Shake vigorously for five minutes. Let stand to settle and collect the aqueous layer. Add a few drops of phenolphthalein and titrate with .05N NaOH.

Add a few drops of phenolphthalein to 200cc of deionized water and titrate with .05N NaOH as a blank.

Grams of Acid = $(V_1 - V_2)$ N(NaOH) (MEq Wt) 1000 liter of Solvent 200

 V_1 = ml of NaOH to neutralize aqueous layer

V2 = ml of NaOH to neutralize blank

N(NaOH) = Normality of NaOH

MEdWt - Milli equivalent weight of CH3COOH

Grams of Acid = $(V_1 - V_2)$ (.05) (.06) 5 liter of Solvent

The maximum acidity allowable is .01%

Moisture Content

An analysis of the percent moisture in the solvent is necessary to qualify its usefulness. A Carl Fischer titration is suitable for this determination. The Organic Section in the Electronics Laboratory is set up for such an analysis.

The maximum water content allowable is 0.3%.

Traces of Metal Impurities

Tests should be made to determine if metal impurities are present in the solvents. Special attention should be focused on Copper and Iron.

If this test shows more than a trace, an analytical analysis is necessary. The Inorganic Section in the Electronics Laboratory is qualified to do this.

EVALUATION OF LACOUER

% Solids Determination of Nitrocellulose Lacquers

On an analytical balance weigh a clean, dry, flat weighing dish with a ground glass cover (approximately 35ml capacity). Pour in approximately 10ml of lacquer and cover immediately. The lacquer depth should not be over 1/8 of an inch. Weigh on an analytical balance and record. Remove the cover and place the dish in a well ventillated oven set at 80°C for 48 hours. Remove and cool to room temperature. Weigh again and record.

Weight of dish = wt. 1

Weight of dish + lacquer = wt.2

Weight of dish + lac. + 48 hrs. at 80°C = wt. 3

% Solids = (wt 3 - wt 1) 100
(wt 2 - wt 1)

Viscosity

A Brookfield viscosity determination on incoming lacquer should be taken. A #3 spindle at 30RPM is the proper range. Care should be taken to submerge the spindle to the proper depth and to keep the lacquer temperature at 25°C. The correct viscosity range is 1800-2200 centipoises.

EVALUATION OF NITROCELLULOSE

Because the lacquer is manufactured by an outside vendor, a sample of the alcohol wet nitrocellulose used in each lacquer batch should be obtained for the following evaluation:

1. Falling Ball Viscosity Determination

The sample of nitrocellulose should be dried for this in a well ventillated oven set at 60°C and the viscosity determination can be made as per Hercules Nitrocellulose Handbook (ASTM D301-33). This gives the viscosity range of the nitrocellulose. The correct range should be 60-80 seconds.

2. Infra Red Analysis

A sample of the alcohol wet nitrocellulose can be sent to Schenectady for infrared spectrographic analysis. This test will show any organic compounds in addition to the nitrocellulose. The sample would have to be dried of alcohol, then made up in a water free solvent to the proper solids concentration. A run on the sample in solution and the solvent alone would be required.

EVALUATION OF PLASTICIZER

A sample of the B-400 plasticizer, Carbon and Carbide, used in the lacquer, should be obtained from the vendor and should compare favorably with the following:

Specific gravity at 20°C	0.991 to 0.996
Refractive index at 20°C	1.4487
Flash point (open cup)	430°F
Maximum acidity	0.05 milliequiv. per gram

Maximum water content

0.25%

V Betar, Bldg. #6 WH Bertrand, Bldg. #6 J Corman, Bldg. #6 IE Halt, BTP ET Peterson, Cleveland

Electronics Park Syracuse, New York June 2b, 1955

Mr. J. Dana Chemical Products Plant 1099 Ivanhoe Rd. Cleveland 10, Ohio

As you requested in your earlier letter submitted with the original lacquer sample, I am forwarding the viscosity measurements made in the factory.

The two liter sample you indicated had a viscosity of 45.3 seconds at 25°C with a no. 7 Parlin cup. With a no. 8 pipet we get a value of 25.9 seconds at 25°C. As you know, this turned out to be slightly below the range of 30-31 second lacquer that we currently are using in production.

To assist us in further viscosity standardization I would very much appreciate the following:

- 1. A 7% solids of the low viscosity (59-61 second R.S.) in H.B. amyl acetate.
- 2. A 7% solids of the medium viscosity (70 second R.S.) in H.B. amyl scetate.
- 3. A 7% solids of the high voscosity (80 second R.S.) in H.B. amyl acetate.

If you could take viscosity readings with the proper Parlin cup and then forward a two liter quantity of each of the three lacquers to us we will obtain our readings for correlation.

This will, I believe, allow us to more closely define our choice of nitrocellulose viscosity within the 60-80 second range.

P.L. Dee

Supervisor

Monochrome Chemical Engineering Unit CATHODE RAY TUBE SUB-DEPARTMENT

PLD: jfe

W. H. Pertrand, Bldg, #6 V. Petar, Bldg, #6 J. M. Gorman, Bldg, #6 I. E. Halt, BTP E. T. Peterson, Cleveland

Electronics Park Syracuse, New York June 15, 1955

Mr. J. Dana General Electric Co. Chemical Products Plant 1099 Ivanhoe Rd. Cleveland 10, Ohio

As agreed in our telephone conversation this morning, the following plan of action on test lacquers will be followed.

A sample of 60-80 second nitrocellulose (7% solids) in high boiling anyl acetate will be the first objective. If filtering this 7% solution proves difficult then two different 4% solids solutions will be formulated, i.e., diluting a quantity of 7% in high boiling amyl acetate to approximately 4% with high boiling amyl acetate would be satisfactory for testing at the Syracuse Tube Plant. Similarly, dilution of a quantity of 7% in high boiling amyl acetate to approximately a 4% solids by using Pearce and Stevens lacquer thinner M-5925 would be necessary for evaluation at Buffalo.

It would be appreciated if we could receive small samples of both the HB and the M-5925 for our own distillation studies.

Paul L. Dee

Supervisor

Monochrome Chemical Engineering Unit CATHODE RAY TUBE SUB-DEPARTMENT

PLD: jfe

W Bertrand, #6
PL Dee, #6
W Highfield, #6
SS Sadowsky, #6
HN Sherwood, #6
LE Swedlund, #6
PN Taggett, #6

Electronics Park Syracuse, New York October 19, 1955

The following is a summary of the lacquer work done during the past four weeks. The effort has been concentrated on the improvement of the present lacquer (FAN Sy-1776), and also on a higher solids butyl acetate lacquer.

Shrinkage records of lacquers A through E are incorporated in daily factory records and the indication is that lacquer B has improved shrinkage somewhat, but it is still below the desired level.

The most promising of the Butyl Acetate lacquers is the 3.5% 18 sec in LLZ butyl acetate and 56% amyl acetate with DRP in the ratio of 2.3 S to IP.

Further work is continuing presently on this lacquer.

Victor Betar

Victor Betar

Monochrome Chemical Engineering Unit CATHODE RAY TUBE SUB-DEPARTMENT

VB:jfe

Formulas

Lac A.

Lac B

Lac C

Lac D

Lac E

1335 cc 6.2 % 18 sec Stock (AA) 465 cc Amyl acetate

720 cc Toluene

720 oc Butyl Acetate

720 cc Butyl Alcohol

32.4 ec DBP

21.6 cc OA

Same as A less 465 cc Amyl Ac.

1335 cc Stock

720 cc Toluene

720 cc Butyl Acetate

720 ce Butyl Alcohol

29.6 cc DBP

19.7 cc OA

Same as C with 35.6 cc DBP and 19.7 cc OA

40 ce Stock

20 cc Toluene

20 cc Dutyl Acetate

20 cc Butyl Alcohol

1.86 cc DBP

1.11 cc OA

			Laco	uer Su	mary			Spots The		0
				*	reak A	£1	198	Kara So Watere So	Ting	Grade
Formula @ 20	% f.l. Solids	Plast	s/p DBP	S/P OA	To the second se	ਰਿਹਾ <u>ਇੰ</u>	1530 1630 1630 1630 1630 1630 1630 1630 16	E de terre	Mottling	2963
Lac A FAN Sy-1776 103	2.2	OA	2.3/1	3.4/1					OK	18
Lac B 105	2.4	DEP	2.3/1	3.4/2					CK	18
Lec C 105	2,4	DBP OA	2,5/1	3.8/1					OK	18
Lac E (40-20-20-20)	2.5	DEP	2.4/1	L:/3.					OK	18
(1.24 DBP)	2.5	DBP	1.8/1	0	1/12	0/12	0/12	0/12	OK	18
40-20-20-20 100 (0.97 DBP)	2,5	DBP	2.3/1	0		yes	yes	yes	OK	18
100% Bu Ac 98	2.3	DEP	2.5/1	0	no	no	yes	no	OK	64
100% Bu Ac 89	2.3	TOP	2.5/1	0	no	no	yes	no	OK	64
100% Bu Ac 92	2.3	DBP TCP	2.5/1	0	no	no	yes	no	OK	6L3
80% Bu Ac 1.0% Am Ac	2.3	EEP TCP	2,3/1	0	no	no	yes	no	OK	64
80% Bu Ac 20% Bu OH	2.3	IRP ICP	2.3/1	0	no	no	mild	no	OK	61,
63% Bu Ac 37% Am Ac	2.3	DBP TCP	2.3/1	0	no	no	yes	no	CK	6L
hlig Bu Ac 112 56% Am Ac	3.5	DBP	2.3/1	0	no l	:/32	no	no 5/1	2 OK	1.8

V. Betar

BAKE OUT TESTS

The bake out tests were conducted inside a metal container on top of a hot plate controlled by a 16 amp, variac. The container was 4" by 6" by 3-1/2". There was no bottom or top to the container. The 4" by 4" plates tested were supported 1-1/2" from the hot plate by four bolts. The container was insulated with asbestos and aluminum foil. A thermometer was positioned 1-1/2" from the surface of the hot plate inside the container. A pyrex glass cover was used to view the bake out. One bolt was removed and an air hose attached to permit the air flush test.

As shown in Chart 2, the film seemed to start burning at approximately 185°C and usually had completed burning at approximately 205°C. The film usually would darken in one small circular area. This darkened area gradually increased in size until the entire plate was covered. The aluminized plates obscured this darkening, but the comparison of the gloss readings on Chart 1 between the control and the baked plates tends to indicate no hindering action due to the aluminum.

Microscopic examination was made after bake out in order to detect any signs of charring. Charring was noticed only on one plate that had a folded film. After baking out for 30 mins. at 205°C, a single charred streak was visible where the film was folded over. The unusual three-fold thickness of the film at this point prevented complete combusion, and the result was a charred streak. No other portion of the film charred.

The use of the Gardner gloss meter as a measure of film presence after bake out is based on the gloss difference between the screen and film (2 and 13).

No difference was noticed between the plate baked out with air flush and those baked without it.

Victor Betar

VB: ch 5/12/55

cc: PL Dee

C Dichter FN Taggett

CHART 1

Screen only	°C Temp	Time-	Color Pale yellow	ardner Gloss Keter 1.5 (Control)
Screen & film	wa.	CO 100	Grayish yellow	13 (Control
	205	30	Fale yellow	2
(air flush)	205	30	Fale yellow	2
	180	30	1/2 Grayish yellow 1/2 Pale yellow	1/2 11 1/2 4
	230	30	Pale yellow	2
Screen and film & aluminized	20.30	Ga-45-	Gray	ll (Control)
	205	30	Bluish gray	7
	300	30	ff ff	8
	200	30	n n	9
	230	30	- 19	7

CHART 2

Screen and film	(Mins) <u>Time</u>	oc Temp
No Air Flush	5 10 20 30 35 37 38 39 40 45	63 69 78 85 154 179 185 - Film started to darken 190 195 - Entire film darkened 196
Air Flush	5 10 15 20 25	60 150 180 - Film started to darken 195 205 - Entire film darkened
Screened, filmed, and aluminized	5 10 15 20 25	50 150 175 - Could not see any darkening 200 210
	5 10 15 20 25 30	50 135 180 - Could not see any darkening 220 270 300

W Bertrand, Bldg. #6 PL Dee, Bldg. #6

Electronics Park Syracuse, New York August 31, 1955

Mr. J. Dana Chemical Products Plant 1099 Ivanhoe Road Cleveland 10, Ohio

Per cent solids determinations and viscosity measurements were made on your lacquers and I am sending you my findings. The per cent solids of the undiluted lacquers were determined by weighing analytically a small portion, and then by reweighing after oven drying for 48 hours @ 80°C. Since my values did not correspond to yours, a second check was made and dried for 96 hours @ 80°C with no change. The per cent solids of the diluted lacquers were calculated values after using the standard factory dilution ratio of 1650 cc stock to 2350 cc of amyl acetate.

As can be seen from the data, the regular factory lacquer (60-80) when diluted from 1650 cc of 7% stock with 2350 cc of amylacetate is 2.88%. This lacquer gives a 60 cp. reading @ 25° G. The three diluted lacquers 3831-59, 69, and 78 all were near 90 cp. @ 25° G.

The present factory filming conditions have favored a fast dry lacquer and all attention has been focused on this. I have tested a series of butyl acetate lacquers and I am sending you the results also. If these lacquers continue to be as good under further testing we may ask your assistance in formulating them.

Victor Betar

Victor Betar Monochrome Chemical Engineering Unit CATHOLE RAY TUBE SUB-DEPARTMENT

VB:jfe attach.

VISCOSITY CHECKS ON CLEVELAND LACS.

As Received	Clev. % Soli	Syr. Lds	Cleve. Visc.	Syr. Graphic Visc. % Solids
383159	7.02	7.60	29.4 Sec #20 @25°C	21.8h, cp. **
3831-69	6.95	7.47	30 Sec #20 @25 [°] G	2160 op.* @25°C
3831-78	6.87	7.20	42.5 Seg #20 @25 ⁸ G	1768 ep.★ @25°C
Reg. Fac. Lac.	437.chma650e	2.88	493.855 Census Trayal	32.5 Sec #8 Pipette @25°C 60 cp.@25°C
Diluted				
3831-59	Ration, St. (Strip)	3,13	MANAGEMENT .	Щ.8 Sec 3.26 922°C #8 Pipette* 91.5 ср. 022°C
3831-69	Alection militaries	3.05	gazdezelejade	147.2 Sec 3.30 @22°C #8** 94.5 cp
3831-78	PARATOLISIANO	2,83		40.6 sec 3.18 @22°C #8* 86.5 cp @22°C @

^{# @25°}C

The lacquer as received from Cleveland was diluted in the usual factory dilution ratio of 1650cc stock lac to 2350 cc of solvent.

The graphic % solids determination was based on previous work where 75 sec nitrocellulose in amyl acetate was plotted showing % solids vs. viscosity (cp.)

^{# #3} spindle @30 RPM

^{🖼 #2} spindle @60 RPM

BUTYL ACETATE LACQUERS

(ua) Brightness	Plasticizor:	C.,	8 Sollds	Dilles	HOJ. GS		ec of Lac.
rempartation	B-jt00	1.4 to 1	2,5	No No	Yes	No No	1.0
eLicetroAcquer»	B-400	2.5 to 1	2,3	Yes	$N_{\mathbf{O}}$	27	1,2
CANADA CANADA	41	87	25	Yes	23	44	11
een Antersaan	tt .	ti .	65	Yes	83	7 9	71
110	B-400	1.3 to 1	17	No	57	11	69
1.07.5	71	11	87	**	17	31	17
AND A PETOMEN	DBP	2.5 to 1	77	1)	Yes	29	65
102	11	#	17	11	No .	11	11
94	91	n	69	Ħ	No	77	**
89	TCP	11	71	No	No	n .	- 63
	101	. 17	11	Yes	11	61	81
		_ *		X			ď
95	TGP & DBP	n -	17	No	!!	91	1.3
90	94 13	5 7	88	17	11	Ħ	1.3
91.	£7 17	71	13	to	Yes	11	1.3

Note: 64 sec. R.S. nitrocellulose was used in all lacquers. TCP # DBP was mixed 1 to 1

Terminology:

B-400 - Flexol B-400 plasticizer

DBP - Dibutyl phthalate

TCP - Tricresy phosphate

S to P - Solids to plasticizer ratio

B-flies - butterflies or bare spots

(incomplete coverage)

- 4 Development Studies of Flotation Filming Lacquers.
 - a) Tank Studies on Lacquers P. L. Dee, V. Betar

A 24 x 24 inch stainless steel tank with a 15-1/2 x 20 inch elliptically shaped frame insert was constructed for the purpose of testing lacquers. The boundary of the insert was as similar as possible to that encountered by the lacquer during the regular film spreading. The depth of the tank was four inches, and the depth of the water cushion used was one inch. The tank was covered by a plexiglass lid with a center hole for lacquer dispensing.

In testing the various types of lacquers, one inch of cushion water (six liters) at 23°C was used. One cc of lacquer was hand dispensed with a pipette. The dry time noted is when a wet glass rod will depress the film 1/4 of an inch without puncturing it and without the film sticking to the rod.

Variations of the following lacquers were tested:

- (1) 4.9% R.S. 18 sec. nitrocellulose in anyl acetate A.R.
- (2) 5.4% H.S. 36 sec. nitrocellulose in amyl acetate A.R. (3) 5.2% H.S. 75 sec. nitrocellulose in amyl acetate A.R.
- (4) 4.9% R.S. 145 sec. nitrocellulose in anyl acetate A.R.

All of the above were plasticized with dibutyl phthalate in the ratio of 1.8 to 1, solids to plasticizer. In certain lacquers, the use of 0.5 cc of octyl acetate per 100 cc of working solution was added for comparison.

The evaporating rate recorded on the data is based on the rate of n-butyl acetate equal to 100.

The above stock solutions were prepared from dried nitrocellulose.

Conclusions:

From the preliminary testing of lacquers made from various grades of nitrocellulose, the following trends are noticed:

Lacquers of high solids content are faster drying than those of lower solids content regardless of nitrocellulose grade.

For each grade of nitrocellulose an optimum percent solids value exists where the spreading area will be the greatest. This is the point where the spreading pressure minus the retarding effect of edge drying is at its maximum.

Octyl acetate in general increases the spreading area of a lacquer and increases its dry time.

Of the lacquers tested, the following have been chosen for more detailed study:

> 1. 4% 18 sec. 2. 4.5% 36 sec 1. 4%

3. 4.5% 75 sec.

4. 3.5% 145 sec.

AREA (Sa.In.)

		A Weds	and the first of t	Carting Contract Contract				
	R.S. Grade	g <u>Solide</u>	Visc (Cps)	Evap Rate	Dry Time (<u>Mins.)</u>	Width	Length	Area
	18 Séc. 18 " 18 " 18 "	4.9 4.0 4.0 3.0 2.5	92.5 52.5 52.5 27.5	59 59 58 59 200	4 7 11 7 (Rauland Lac)	15-1/2 15-1/2 15-1/2 15-1/2 15-1/2	16 19 19 17 20	248 294 294 * 263 310
	36 " 36 " 36 "	5.4 4.5 4.5 4.0	338 220 220 147	59 59 59 59	3 8 11 7	15-1/2 15-1/2 15-1/2 15-1/2	17 16 19 15	263 248 294 * 232
	75 " 75 " 75 " 75 "	5.2 4.5 4.5 4.0 2.9	450 280 280 170 60	59 59 59 59 70	3 4 11 11 *	15 15 15 15 15	17 18 19 19	255 270 285 * 285 * 285 *
1	145 " 145 " 145 " 145 "	4.9 4.0 3.5 3.0 2.0	556 270 175 105 35	59 59 59 59 59	3 11 10 14	14 15-1/2 15-1/2 15-1/2	15 19 19 20 16	210 294 294 310 224

^{*} Added 0.5cc of actyl acetate per 100cc of lacquer.

LACQUER

b) Aging Effect on Lacquer - P. L. Dee, V. Betar

The method used to evaluate the effective power of various ester solvents on nitrocellulose is the toluene tolerance test. Nitrocellulose lacquers from such solvents can tolerate additions of toluene (a non-solvent) up to a certain point, after which gelling occurs. Localized gelling takes place at the tip of the burette delivering toluene to the mixture, even though mechanical stirring is used. As an arbitrary end point, a one-minute time limit was set on the disappearance of the gel. That is, toluene was added until the first signs of gelling, then, one ml. additions were added every minute, with stirring, until the gel failed to disappear.

Toluene tolerance titrations were made on six types of nitrocellulose lacquers diluted to a 3% solids consistency with:

- 1. Pierce & Stevens lacquer thinner.
- 2. Commercial solvents Amyl Acetate (H.B.)
- 3. Malinkrodt Amyl Acetate (A.R.)

The tests attempted to find the effect of time upon the solvency power of each solvent used.

Each of the lacquers was made to a 7% and 4% solids content with 70 sec. nitrocellulose (R.S.) in each of the three solvents above. The 7%

solids lacquer was chosen to approximate the present incoming lacquer from Raffi and Suanson. The 4% solids lacquer was chosen for comparison tests.

At various intervals, these stock lacquers were diluted to a 3% solution with each solvent type. A 25cc amount of each of these 3% solutions was then titrated with toluene as described. The first titration (O days) was made after the stock lacquers were mixed and had rolled for 72 hours. The time schedule of the other titrations was based on the first titration being zero days.

Brookfield viscosity readings were taken on the stock solutions at the time of each toluene titration.

Toluene titrations of 7% stock lacquers diluted to 3% with methyl ethyl ketone and methyl isobutyl ketone were also taken, and the results are listed in the data.

Conclusions:

No pronounced effect is noticed in toluene titrations on lacquer solutions for the duration of the test. The trend, however, is for the titrations to level off after the second week. The viscosities recorded seem to fall into this same trend except for the readings at 27 and 57 days. The unexpected increase in the viscosities of the 7% lacquer at 27 days was probably due to an increased submersion of the Brookfield spindle. The slight decrease in the 7% lacquer readings at 57 days was probably due to a 1/2 degree temperature reading error.

The leveling trend of the toluene titrations and viscosities after two weeks indicates that this period is the minimum time requirement for the complete solvency of the lacquer. A period of one month would provide a slight safety factor.

The 7% to 3% dilution seems to produce slightly higher toluene tolerances than the 4% to 3% dilution. However, the lack of erratic fluctuations in the 4% to 3% tolerance and viscosity readings would favor the use of a 4% stock lacquer as the incoming material.

Based on the viscosity tests, the Pierce and Stevens lacquer thinner, which is approximately two parts amyl acetate to one part butyl acetate, would appear to be the more active solvent of the investigation.

Based on the toluene tolerance tests, much better solvent action can be expected from faster evaporators such as methyl isobutyl ketone and methyl ethyl ketone, but their effects on a lacquer film would limit their usefulness. The analytical reagent anyl acetate would more often impart a slightly greater tolerance than either the Pierce and Stevens thinner or the commercial solvents anyl acetate. The differences become less and less after two weeks. The choice of solvent, assuming uniformity from barrel to barrel, could easily be determined by current price quotations.

		O Day Visc. 20°C		<u>5 Da</u> Visc. 20°C	YS Ml. Tol.	13 Da Visc. 21.5°C	1.1.	27 D: Visc. 22°C	Ays Ml. Tol.	57 D Visc. 23°C	eye Ml. Tol.	120 D Visc. 22°C	ಬರೆತೆಯಲಕರು
7% P&S 3% with 3% with 3% with	CSAA	2600	* 64 66 68	2340	68 66 68	2280	68 66 68	2320	72 70 70	2120	70 68 68	2260	73 69 68
7% CSAA 3% with 3% with 3% with	CSAA	2860	64 65 70	2640	68 66 70	2584	68 66 70	2640	69 67 70	2460	68 67 69	2540	69 69
7% AA 3% with 3% with 3% with		2772	70 66 70	2608	70 67 70	2496	68 66 68	2500	69 67 69	2320	68 66 69	2440	68 68 69

*Viscosity in centipoises

	O Days Visc. 20°C Tol.	5 Days Visc. 20°0 Tol.	13 Days Visc. 21.5°0 Tol.	27 Days Visc . 22 ⁰ C Tol.	visc, 23°0 Tol	120 Days Visc. 22°C Tol.
4% P&S	363	355	34 2	340	300	327
3% with P&S	61	64	64	66	65	66
3% with ISAA	62	65	64	66	65	67
3% with AA	64	66	66	68	66	68
4% CSAA	430	412	408	396	360	387
3% with 1%S	63	64	64	65	64	66
3% with CSAA	63	63	63	64	63	68
3% with AA	62	63	63	64	62	66
4% AA	405	380	356	355	330	342
3% with P&S	61	64	63	64,	63	65
3% with CSAA	64	65	64	64	62	67
3% with AA	66	67	66	66	64	67

Viscosity Conversions to 2000

	O Days	5 Days	13 Days	27 Days	57 Days	120 Days
7% Pes	2600	2340	2395	2470	2355	2410
7% CSAA	2860	2640	2699	2790	2695	2690
7% AA	2772	2608	2611	2650	2555	2590
LE PES	363	355	342*	340*	300*	327*
4% CSAA	430	412	408*	396*	360*	387*
4% AA	405	380	356*	355*	330*	342*

Note: Readings are in centipoises.

P&S = Pierce & Stevens lacquer thinner

CSAA= Commercial solvents anyl acetate (H.B.)

AA = Malinkrodt amyl acetate (A.R)

*These readings are at the temperatures listed on page 13.

			O Days	6 Days
Stock	Dilution	With	ml Toluene	ml Toluene
7% CSAA	3%	50-50 IPA + MEK	104	
7% AA	3%	11	105	
76 P&S	3%	F 9	108	
45 CSAA	3%	II II	84	
4% AA	3%	19	85	
4% Pas	3%	**	86	
7% CSAA	3%	MEK	118	120
7% AA	3%	MEK	121	123
7% P&S	3%	MEK	120	122
7% CSAA	3%	MIBK	98	1.00
7% AA	3%	MIBK	103	104
7% P&S	3%	MIBK	102	104

Note: 25 ml samples were used in titrations.

IPA = Iso propyl alcohol
MEX = Methyl Ethyl Ketone
MIEK = Methyl Iso butyl Ketone

c) Combined Screening and Filming - F. L. Dee

Through a period of nearly four weeks of three-shift operation a filming defect, bare spots in the corners of the screen, has been the largest single cause of shrinkage.

From extensive observations of this defect at the pouroff platform, the film appears wet in the center and dry along the edges. In other words, when spreading the film on what is in effect an elliptical shaped plane, the lacquer adequately covers an area out to the end of the minor axis. At this point the lacquer reflects off the glass wall on each boundary of the short axis and partically folds or runs back on itself. This pattern which has been observed at lacquer dispensing leads to irregular areas on the pouring edge but more harmful is the extra thickness of film and its wetness. In contrast, the lacquer just spreads cut to the extremities of the major axis and in so doing is thinned out sufficiently to be considerably drier than lacquer at the end of the minor axis.

The low viscosity and volatile solvents in this lacquer actually accentuate a condition that is present with any lacquer cast on this type of plane. The center to edge wet and dry variation is so magnified, however, with this lacquer that normal tolerances are sharply reduced.

As a result, the water to pipette distance, the timing and quantity of lacquer, referencing of dispenser and other variables, such as temperature, require degrees of exactness that are becoming more extreme as additional process knowledge is obtained.

In attempts to keep within the present system, some eight minor changes have been made in the current lacquer. These involved small variations in plasticizer or ratios of stock solution to diluting solvent. It is significant that in all such lacquer modification tests the resultant product was poorer than the lacquer it was meant to correct.

It would appear then that a different type lacture could be of value in allowing wider tolerances in actual processing. Development work for some has been directed toward this goal, and as promising lacquers arise, they will be tested under actual process conditions.

- 5 Color and Brightness Control F. D. Gordon
 - a) Phosphor Lot Approval.

Seven phosphor lots were tested for color and brightness during Lurch for both the Syracuse and Buffalo Tube plants. As per the 5.1., readings of four tubes per 2,000 lb. lot were made using the laboratory spectroradiometer. The results are listed below—all readings are average values of the CIE color coordinates and brightness.

PROGRESS REPORT NO. 6 (D.A. 30113)

TITLE: Filming Investigations - Triphenyl Phosphate Plasticizer

PERSONNEL ASSIGNED: Paul L. Dee

PROGRESS FROM: January 15, 1953 to February 27, 1953.

FOREWARD:

This Progress Report is a compilation of past work using Triphenyl Phosphate Plasticizer. Although separate reports have been issued covering the majority of this work, the data is collected here for review and future planning.

The accompanying sheet shows the brightness and life test results on special aluminized 27EP4°s that had been flotation filmed with lacquer containing 0.4 gms. of Tri-Phenyl Phosphate Plasticizer per 50 cc°s of solution. The control tubes, also 27EP4°s, had the regular B-400 Plasticizer in the lacquer (1.0 c.c. per 50) for their filming operation.

This work was prompted by the reduced brightness of factory 27EPL's, a condition that was first suspected by noting the excessive mottling in the film at light inspection. It was believed that the B-400 Plasticizer which takes up 3.3% water by weight was the principal cause for film blemishes and decreased brightness in a finished tube. Our present lacquer suppliers, Raffi and Swanson, had suggested Tri-Phenyl Phosphate among other plasticizers as a possible means of getting around this water absorption problem. The increased brightness with Tri-Phenyl Phosphate lacquer bears out the wisdom of their suggestion.

There are, however, certain processing problems that have arisen in using lacquer containing this new plasticizer. A slightly thinner film is east when the same volume of lacquer that is used with B-400 solutions is dispensed, judging from the interference colors at pouroff. Increasing the amount of lacquer in part compensates for this, but the Tri-Phenyl Phosphate films set up much faster and are ready for pouroff of cushion water in approximately two-thirds of the time that B-400 films require. Literally presaturating the water 1-2 seconds before dispensing this new plasticized lacquer did not lengthen the setting time sufficiently. For this reason small amounts of octyl acctate were added to the lacquer to increase the set up time. While this proved successful, it resulted in a drop in brightness. Additional work with the octyl acetate (Specials 4 & 5) would indicate there is an optimum amount for lacquer containing the 0.4 gms. of Tri-Phenyl Phosphate that will yield consistently bright tubes.

This rather roundabout approach to convenient set up time has been necessary because of limitations at where lacquer can be dispensed on the conveyor.

Future work is planned for increasing the amount of Tri-Phenyl Phosphate and also continuing a study of octyl acetate. A larger volume of tubes will also bear out or refute an unanswered question on film flexibility with the Tri-Phenyl Phosphate.

Life test racks were very limited during the course of these tests (Jan. 20, 1953 to Feb. 27, 1953) and while the controls were not put on life, regular factory production life test results are listed here for comparison.

Paul L. Dee Materials & Processes CATHODE-RAY TUBES

PLD:f

Distribution: VCC

A.F.Carl - B.T.P.

GLC

HJElias - B.T.P. IEHalt - B.T.P.

JW Wright - B.T.P.

SUMMARY OF PAST WORK USING TRI-PHENYL PHOSPHATE PLASTICIZER IN FILMING SOLUTION

27EP4

	I _b @ 20 ft.1.				500 Hrs.					
		500 Hrs.			Cut Off	Is	50V I _S	% Orig.	Gas Ratio	Screen
SPECIAL-1	106 ua	115 ua			46	1100	1254	95	.005	OK
II _2	120	130	* a		50	1150	1150	88.5	.02	OK
3	104	110			36	760	1246	92.6	٥02	OK
4	133	GD.					Not	On Life		
5	120	5			54	1220	1086	86.1	.22	OK
CONTROL-1	135	cons					Not	On Life*		
2	126	•					. 11	st tt		
3	126						11	u 11		
4	145	449					11	11		
5	145.5	da.					11	ft ft		

*Life Test Racks Not Available.

All Specials had 0.4 gms. of Tri-Phenyl Phosphate per 50 c.c. of lacquer. Special - 4 in addition had 2.0 c.c. of octyl acetate per 50 c.c. of solution. Special - 5 in addition had 1.5 c.c. of octyl acetate per 50 c.c. of solution.

Regular Factory Production 27EP4's Showed the Following Life Test Results:

		Hours	50V	% Orig.	Gas Ratio	Screen
Jan.	Production	788	1311	98.7	.01	OK
Jan.	Production	1100	1280	93.7	.01	OK
Feb.	Production	805	1295	98.8	°01	OK
Feb.	Production	306	936	71.7	.01	OK